

## Theoretical Evaluation of the Overall Values of Discrepancy Indices for Truncated Data.

### I. Normalized *R* indices for a Centrosymmetric Crystal with Similar Atoms

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#### Abstract

Theoretical expressions for the local values of six types of normalized *R* indices applicable to truncated data are derived for a centrosymmetric crystal by taking the model structure to be of the imperfectly related incomplete type. These indices are tabulated as functions of  $\sigma_4$  and  $y_t$ . These results can be used to obtain the overall values of the *R* indices applicable to truncated data which is characterized by a given value of  $y_t$ .

#### 1. Introduction

Values of different types of discrepancy indices (*i.e.* *R* indices) have been worked out in the literature for a number of crystallographic situations, such as crystals with similar atoms, crystals with heavy atoms, crystals with pseudo-symmetry in the atomic distribution, *etc.* (for details see Srinivasan & Parthasarathy, 1976, and the review of Parthasarathy, 1975). These results were obtained under the assumption that all the independent reflections in a given range of  $(\sin \theta/\lambda)$  (*e.g.* Cu  $K\alpha$  sphere) are available in the data. However, in actual crystals, the observed intensity of a certain percentage of reflections may be negative and many crystallographers truncate the data sets by omitting such reflections as well as those whose net counts are less than one to two times the standard deviation of this value (Stout & Jensen, 1968). Hence, it would be useful to evaluate theoretically the overall values of the various *R* indices applicable to such *truncated* data, wherein the reflections for which  $y_N < y_t$  ( $= \sqrt{z_t}$ ) are omitted.<sup>†</sup> In this series of papers we shall therefore derive the theoretical expressions of the various *R*

indices corresponding to different crystallographic situations and show how these results could be used to compute their theoretical *overall values*. Since the various indices behave differently under different situations (Parthasarathy & Parthasarathi, 1975; Parthasarathi & Parthasarathy, 1977; PP, 1977 hereafter), we shall deal with all the *R* indices in this series.

In this series we shall mostly follow the notations used in chapters 5 and 6 of Srinivasan & Parthasarathy (1976; hereafter SP, 1976). We shall use the abbreviations *C* and *NC* to denote the centrosymmetric and non-centrosymmetric cases respectively. We shall denote the joint probability density function (joint p.d.f. hereafter) of the normalized structure amplitudes  $y_N$  and  $y_P^c$  valid for the complete data by  $P(y_N, y_P^c)$  and that valid for the truncated data by  $P_t(y_N, y_P^c)$ . For convenience we shall refer to  $P_t(y_N, y_P^c)$  as the truncated distribution function. The expectation value of  $f(y_N, y_P^c)$  for the truncated data will be denoted by  $\langle f(y_N, y_P^c) \rangle_t$  and that for the complete data by  $\langle f(y_N, y_P^c) \rangle$ .

The experimental value of an *R* index is usually computed by taking all the independent observed reflections as a single group. We refer to the value of the *R* index thus obtained as the *overall value* of the *R* index. A number of factors, such as the positional errors in the atoms in the model, lack of similarity of the atoms in the unit cell, *etc.*, cause the value of an *R* index for a general model to vary with  $\sin \theta/\lambda$ . The theoretical evaluation of the overall value of an *R* index is therefore generally carried out in two stages; namely, (i) evaluation of the *R* index in different narrow regions of  $\sin \theta/\lambda$  (within which the atomic scattering factors can be treated as constant) and (ii) evaluation of the overall value by taking care of the factors which change with  $\sin \theta/\lambda$  (*e.g.* atomic scattering factors) and by giving proper weights depending on the number of observed reflections in the various ranges. We shall therefore refer to the value of an *R* index calculated using reflections in a narrow range of  $\sin \theta/\lambda$  as a *local value* of the *R* index in order to distinguish it from its overall value. The overall value of an *R* index will be

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† For convenience, we shall refer to the data which consist of all the theoretically possible independent reflections within a given region of  $(\sin \theta/\lambda)$  as the *complete data* and the data which exclude the reflections for which  $y_N < y_t$  as the *truncated data*.

denoted with a bar over the corresponding symbol, while the local value of the index will be denoted without the bar.

In this paper we shall obtain, for a centrosymmetric crystal, the theoretical expressions for the local values of the six normalized  $R$  indices,\* *viz.*  $R_1(F)$ ,  $R_1(I)$ ,  $R_1^*(F)$ ,  $R_1^*(I)$ ,  $R_1^f(F)$  and  $R_1^f(I)$  and show how these could be used to evaluate the overall values of these indices.

## 2. Derivation of the theoretical expressions for the overall values of the normalized $R$ indices

### 2.1. Preliminary results

We shall presently explain the general notation and nomenclature regarding the overall values of different types of  $R$  indices computed for truncated data by taking the conventional normalized index  $R_1(F)$  as an illustrative example. The corresponding results for the other indices can be similarly obtained.

The overall value of the conventional normalized index  $R_1(F)$  applicable to the complete data is defined to be (SP, 1976)

$$\bar{R}_1(F) = \frac{\sum_{hkl}^t |F_N| - |F_P^c|/\sigma_1}{\sum_{hkl}^t |F_N|}, \quad (1)$$

where the summation is over *all* the theoretically possible independent reflections within a given  $(\sin \theta/\lambda)$  range† ( $0 \leq s \leq S_{\max}$ , say),  $|F_P^c|$  is the magnitude of the calculated structure factor of the trial structure consisting of  $P$  out of  $N$  atoms in the unit cell and  $|F_N|$  is the magnitude of the structure factor of the crystal structure. Here  $\sigma_1^2$  is defined to be‡

$$\sigma_1^2 = \langle |F_P^c|^2 \rangle / \langle |F_N|^2 \rangle = \sigma_P^2 / \sigma_N^2. \quad (2)$$

For a structure with similar atoms

$$\sigma_1^2 = P/N, \quad (3)$$

which is a constant independent of  $\sin \theta/\lambda$ . The overall value of this index computed with the truncated data is

denoted by  $[\bar{R}_1(F)]_t$  and is defined to be

$$[\bar{R}_1(F)]_t = \frac{\sum_{hkl}^t |F_N| - |F_P^c|/\sigma_1}{\sum_{hkl}^t |F_N|}, \quad (4)$$

where  $\sum_{hkl}^t$  means that the summation is over the independent reflections of the *truncated* data in the range 0 to  $S_{\max}$ . In our theoretical studies, it is convenient to use the normalized variables  $y_N$  and  $y_P^c$  defined by

$$y_N = |F_N|/\sigma_N, y_P^c = |F_P^c|/\sigma_P. \quad (5)$$

Making use of (5), we can rewrite (4) as

$$[\bar{R}_1(F)]_t = \frac{\sum_{hkl}^t \sigma_N |y_N - y_P^c|}{\sum_{hkl}^t \sigma_N y_N}. \quad (6)$$

If the reflections are divided into groups based on the values of  $s$ , we can rewrite (6) as

$$[\bar{R}_1(F)]_t = \frac{\sum_s \sum_r^t \sigma_{Nsr} |y_N - y_P^c|_{sr}}{\sum_s \sum_r^t \sigma_{Nsr} y_{Nsr}}, \quad (7)$$

where the summation over  $r$  is carried out over the reflections in a given range of  $\sin \theta/\lambda$  and over  $s$  is carried out over the various ranges into which the interval 0 to  $S_{\max}$  has been partitioned. Here  $\sigma_{Nsr}$  denotes the value of  $\sigma_N$  for reflection  $r$  in the range  $s$ . If the  $\sin \theta/\lambda$  ranges are sufficiently narrow, we can take the values of  $\sigma_{Nsr}$  for the different reflections in the range  $s$  to be the same ( $\sigma_{Ns}$ , say). We can therefore rewrite (7) as

$$[\bar{R}_1(F)]_t = \frac{\sum_s \sigma_{Ns} \sum_r^t |y_N - y_P^c|_{sr}}{\sum_s \sigma_{Ns} \sum_r^t y_{Nsr}}, \quad (8)$$

If  $n_s$  is the number of *observed* independent reflections in the range  $s$  in the truncated data we can write (8) as

$$[\bar{R}_1(F)]_t = \frac{\sum_s \sigma_{Ns} n_s [\langle |y_N - y_P^c| \rangle_s]_t}{\sum_s \sigma_{Ns} n_s [\langle y_N \rangle_s]_t}, \quad (9)$$

where  $[\langle |y_N - y_P^c| \rangle_s]_t$  and  $[\langle y_N \rangle_s]_t$  denote respectively the expectation values of  $|y_N - y_P^c|$  and  $y_N$  for the observed reflections in the range  $s$  of the truncated data.

\* We shall not consider the indices  $R_1^*(F)$  and  $R_1^*(I)$  since  $R_1^f(F)$  and  $R_1^f(I)$  are somewhat better than the former two (PP, 1977).

† We shall use  $s$  to stand for  $\sin \theta/\lambda$ .  $S_{\max}$  is the maximum value of  $s$  for the given data.

‡ We shall denote  $1 - \sigma_1^2$  by  $\sigma_2^2$ .

Table 1. Definition of the overall values of various normalized  $R$  indices for truncated data and related results

Number	Name of the $R$ index	Notation for the overall value of the index	Overall value of the index		Definition of the local value of the unnormalized indices based on the normalized variables $y_N$ and $y_P^c$
			Definition*	Equivalent expression	
1	Conventional index based on $F$	$[\bar{R}_1(F)]_t$	$\frac{\sum_t  F_N  -  F_P^c /\sigma_1}{\sum_t  F_N }$	$\frac{\sum_s f_s n_s [R_1(y)]_t}{\sum_s f_s n_s}$	$[R_1(y)]_t = \frac{\langle  y_N - y_P^c  \rangle_t}{\langle y_N \rangle_t}$
2	Conventional index based on $I$	$[\bar{R}_1(I)]_t$	$\frac{\sum_t  I_N - I_P^c/\sigma_1^2 }{\sum_t I_N}$	$\frac{\sum_s f_s^2 n_s [R_1(z)]_t}{\sum_s f_s^2 n_s}$	$[R_1(z)]_t = \frac{\langle  y_N^2 - (y_P^c)^2  \rangle_t}{\langle y_N^2 \rangle_t}$
3	Booth-type index based on $F$	$[{}_B\bar{R}_1(F)]_t$	$\frac{\sum_t ( F_N  -  F_P^c /\sigma_1)^2}{\sum_t  F_N ^2}$	$\frac{\sum_s f_s^2 n_s [{}_B R_1(y)]_t}{\sum_s f_s^2 n_s}$	$[{}_B R_1(y)]_t = \frac{\langle (y_N - y_P^c)^2 \rangle_t}{\langle y_N^2 \rangle_t}$
4	Booth-type index based on $I$	$[{}_B\bar{R}_1(I)]_t$	$\frac{\sum_t (I_N - I_P^c/\sigma_1^2)^2}{\sum_t I_N^2}$	$\frac{\sum_s f_s^4 n_s [{}_B R_1(z)]_t}{\sum_s f_s^4 n_s}$	$[{}_B R_1(z)]_t = \frac{\langle (y_N^2 - (y_P^c)^2)^2 \rangle_t}{\langle y_N^2 \rangle_t}$
5	Fractional-type index based on $F$	$[\bar{R}_1^f(F)]_t$	$\frac{1}{N_0} \sum_t \left  \frac{ F_N  -  F_P^c /\sigma_1}{( F_N  +  F_P^c /\sigma_1)/2} \right $	$\frac{\sum_s n_s [R_1^f(y)]_t}{\sum_s n_s}$	$[R_1^f(y)]_t = 2 \left\langle \left  \frac{y_N - y_P^c}{y_N + y_P^c} \right  \right\rangle_t$
6	Fractional-type index based on $I$	$[\bar{R}_1^f(I)]_t$	$\frac{1}{N_0} \sum_t \left  \frac{I_N - I_P^c/\sigma_1^2}{(I_N + I_P^c/\sigma_1^2)/2} \right $	$\frac{\sum_s n_s [R_1^f(z)]_t}{\sum_s n_s}$	$[R_1^f(z)]_t = 2 \left\langle \left  \frac{y_N^2 - (y_P^c)^2}{y_N^2 + (y_P^c)^2} \right  \right\rangle_t$

\* The summation  $\sum_t$  is over the independent reflections of the truncated data. The summation  $\sum_s$  is over the different narrow ranges of  $\sin \theta/\lambda_0$ .  $N_0$  is the number of reflections in the truncated data.

Since  $[\langle y_N \rangle_s]_t$  is a property of the structure but not of the model and since for a structure with similar atoms† the p.d.f. of  $y_N$  is independent of  $s$  (Wilson, 1949), it follows that  $[\langle y_N \rangle_s]_t$  will depend only on  $y_t$ . Hence we can write  $[\langle y_N \rangle_s]_t$  simply as  $[\langle y_N \rangle]_t$ . We can therefore rewrite (9) as

$$[\bar{R}_1(F)]_t = \frac{\sum_s n_s \sigma_{Ns} [R_1(y)]_t}{\sum_s n_s \sigma_{Ns}}, \quad (10)$$

where  $[R_1(y)]_t$  is defined to be

$$[R_1(y)]_t = \frac{\langle |y_N - y_P^c| \rangle_s]_t}{[\langle y_N \rangle]_t}. \quad (11)$$

We refer to  $[R_1(y)]_t$  as the local value of  $R_1(y)$  calculated with the observed reflections in a particular range  $s$ . For equal-atom structures,  $\sigma_N = \sqrt{Nf}$ . We can therefore rewrite (9) as

$$[\bar{R}_1(F)]_t = \frac{\sum_s f_s n_s [R_1(y)]_t}{\sum_s f_s n_s}. \quad (12)$$

It is clear from (12) that we can evaluate the overall value  $[\bar{R}_1(F)]_t$  for the truncated data in  $0 \leq s < S_{\max}$  if we know, corresponding to the various ranges of  $s$ , the values of the scattering factor of the atom, the number of independent reflections in the truncated data and the local values of  $[R_1(y)]_t$ . Of these,  $f_s$  and  $n_s$  for a given crystal are known quantities; we shall show in the rest of this paper how the local values  $[R_1(y)]_t$  and those for the other normalized  $R$  indices can be obtained theoretically.

As stated earlier, the above considerations can be carried over to the other five normalized  $R$  indices. The final expressions which are the analogues of (12) are hence listed in Table 1 without derivation.

## 2.2. Derivation of the joint p.d.f. of $y_N$ and $y_P^c$ for the truncated data

It is seen from columns 5 and 6 of Table 1 that the overall values of the various normalized  $R$  indices can be calculated if we obtain the expectation values of simple functions of  $y_N$  and  $y_P^c$ . Thus the overall values of these  $R$  indices can, in principle, be evaluated if we know the joint p.d.f. of  $y_N$  and  $y_P^c$  for the truncated data, i.e. the function  $P_t(y_N, y_P^c)$ . It is clear that the function

† For a structure with heavy atoms the p.d.f. of  $y_N$  involves the parameter  $\sigma_1^2$ . Since  $\sigma_1^2$  is a function of  $s$ , it follows that  $[\langle y_N \rangle_s]_t$  could also depend on  $s$ .

$P_t(y_N, y_P^c)$  is related to the function  $P(y_N, y_P^c)$  by

$$P_t(y_N, y_P^c) = \frac{1}{\beta} P(y_N, y_P^c), \quad y_t \leq y_N < \infty \quad (13)$$

$$0 \leq y_P^c < \infty,$$

where  $\beta^*$  is given by

$$\beta = \int_{y_t}^{\infty} \int_0^{\infty} P(y_N, y_P^c) dy_N dy_P^c. \quad (14)$$

The function  $P(y_N, y_P^c)$  for the C case is known to be (SP, 1976)

$$P(y_N, y_P^c) = \frac{2}{\pi \sigma_B} \exp \left\{ -\frac{[y_N^2 + (y_P^c)^2]}{2\sigma_B^2} \right\}$$

$$\times \cosh \left[ \frac{\sigma_A y_N y_P^c}{\sigma_B^2} \right],$$

$$0 \leq y_N < \infty, \quad 0 \leq y_P^c < \infty, \quad (15)$$

where

$$\sigma_A^2 + \sigma_B^2 = 1, \quad \sigma_A = \sigma_1 D \quad (16)$$

$$D = \exp \left( -\frac{\pi^3}{4} |H|^2 \langle |\Delta r| \rangle^2 \right), \quad |H| = 2s. \quad (17)$$

Making use of (15) and (16), we have shown {in the Appendix† [see (A-10)]} that  $\beta_C$  is given by

$$\beta_C = \operatorname{erfc} (y_t / \sqrt{2}). \quad (18)$$

From (13) and (15), we obtain

$$P_t(y_N, y_P^c) = \frac{2}{\beta_C \pi \sigma_B} \exp \left\{ -\frac{[y_N^2 + (y_P^c)^2]}{2\sigma_B^2} \right\}$$

$$\times \cosh \left[ \frac{\sigma_A y_N y_P^c}{\sigma_B^2} \right],$$

$$y_t \leq y_N < \infty, \quad 0 \leq y_P^c < \infty. \quad (19)$$

### 2.3. Derivation of the theoretical expressions for the local values of normalized R indices applicable to truncated data

*Index*  $[R_1(y)]_t$ . From the definition of  $[R_1(y)]_t$  in Table 1, we have

$$[R_1(y)]_t = \frac{1}{\langle y_N \rangle_t} \int_{y_t}^{\infty} \int_0^{\infty} |y_N - y_P^c| P_t(y_N, y_P^c) dy_N dy_P^c, \quad (20)$$

\* Since the function  $P(y_N, y_P^c)$  for the C and NC cases is different,  $\beta$  will be different for the two cases. Hence, the quantity appropriate to the C and NC cases will be denoted by  $\beta_C$  and  $\beta_{NC}$  respectively.

† This appendix has been deposited with the British Library Lending Division as Supplementary Publication No. SUP 35848 (7 pp.). Copies may be obtained through The Executive Secretary, International Union of Crystallography, 5 Abbey Square, Chester CH1 2HU, England.

where  $P_t(y_N, y_P^c)$  is given by (19). Making use of (13), we can rewrite (20) as

$$[R_1(y)]_t = \frac{\langle y_N \rangle}{\beta_C \langle y_N \rangle_t} \left[ \frac{1}{\langle y_N \rangle} \int_0^{\infty} \int_0^{\infty} |y_N - y_P^c| P(y_N, y_P^c) \right.$$

$$\times dy_N dy_P^c - \frac{1}{\langle y_N \rangle} \int_0^{\infty} \int_0^{\infty} |y_N - y_P^c|$$

$$\times P(y_N, y_P^c) dy_N dy_P^c \left. \right]. \quad (21)$$

The first term within the square brackets in (21) represents  $\langle |y_N - y_P^c| \rangle / \langle y_N \rangle$ , which by definition is  $R_1(y)$ . It has been shown that (SP, 1976)

$$R_1(y) = [2(1 + \sigma_A)]^{1/2} + [2(1 - \sigma_A)]^{1/2} - 2. \quad (22)$$

Making use of the known result that  $\langle y_N \rangle = \sqrt{2/\pi}$  (Wilson, 1949) and the expressions for  $\beta_C$  [see (18)] and  $\langle y_N \rangle_t$  [see (A-11)], we can rewrite (21) as

$$[R_1(y)]_t = \exp(y_t^2/2) \left[ R_1(y) - \sqrt{\frac{\pi}{2}} \int_0^{\infty} \int_0^{\infty} |y_N - y_P^c| \right.$$

$$\times P(y_N, y_P^c) dy_N dy_P^c \left. \right]. \quad (23)$$

It is convenient to change the variables of integration to  $u$  and  $v$  where

$$u = y_N / (1 + y_N) \quad \text{and} \quad v = y_P^c / (1 + y_P^c). \quad (24)$$

Thus, we obtain

$$[R_1(y)]_t = \exp(y_t^2/2) \left[ R_1(y) \right.$$

$$- \sqrt{\frac{\pi}{2}} \int_0^{y_t/(1+y_t)} \int_0^1 \left| \frac{u}{1-u} - \frac{v}{1-v} \right|$$

$$\times P \left( \frac{u}{1-u}, \frac{v}{1-v} \right)$$

$$\times \frac{du}{(1-u)^2} \frac{dv}{(1-v)^2} \left. \right]. \quad (25)$$

Here,  $P[u/(1-u), v/(1-v)]$  means that in expression (15) for  $P(y_N, y_P^c)$ ,  $y_N$  is to be replaced by  $u/(1-u)$  and  $y_P^c$  by  $v/(1-v)$ .

*Index*  $[R_1(z)]_t$ . From the definition of  $[R_1(z)]_t$  in Table 1 we have

$$[R_1(z)]_t = \frac{1}{\langle y_N^2 \rangle_t} \int_{y_t}^{\infty} \int_0^{\infty} |y_N^2 - (y_P^c)^2| P_t(y_N, y_P^c) dy_N dy_P^c. \quad (26)$$

Following the method used for  $[R_1(y)]_t$  and using (A-13) and the definition (see SP, 1976)

$$R_1(z) = \langle |z_N - z_P^c| \rangle = \langle |y_N^2 - (y_P^c)^2| \rangle,$$

we can rewrite (26) as

$$\begin{aligned} [R_1(z)]_t &= \left[ R_1(z) - \int_0^{y_t/\infty} \int_0^{\infty} |y_N^2 - (y_p^c)^2| \right. \\ &\quad \times P(y_N, y_p^c) dy_N dy_p^c \Big] \\ &\quad \times [\beta_C + \sqrt{(2/\pi)} y_t \exp(-y_t^2/2)]^{-1}. \end{aligned} \quad (27)$$

It is known that (SP, 1976)

$$R_1(z) = \frac{4}{\pi} \sigma_B. \quad (28)$$

Making use of the substitution (24), we can rewrite (27) as

$$\begin{aligned} [R_1(z)]_t &= \left[ R_1(z) - \int_0^{y_t/(1+y_t)} \int_0^1 \left| \left( \frac{u}{1-u} \right)^2 \right. \right. \\ &\quad \left. \left. - \left( \frac{v}{1-v} \right)^2 \right| P\left( \frac{u}{1-u}, \frac{v}{1-v} \right) \right. \\ &\quad \times \frac{du}{(1-u)^2} \frac{dv}{(1-v)^2} \Big] \\ &\quad \times [\beta_C + \sqrt{(2/\pi)} y_t \exp(-y_t^2/2)]^{-1}. \end{aligned} \quad (29)$$

*Index*  $[{}_B R_1(y)]_t$ . From the definition of  $[{}_B R_1(y)]_t$  given in Table 1 we can obtain

$$[{}_B R_1(y)]_t = \frac{\langle y_N^2 \rangle_t + \langle (y_p^c)^2 \rangle_t - 2\langle y_N y_p^c \rangle_t}{\langle y_N^2 \rangle_t}. \quad (30)$$

Substituting for  $\langle y_N^2 \rangle_t$ ,  $\langle (y_p^c)^2 \rangle_t$  and  $\langle y_N y_p^c \rangle_t$  from (A-13), (A-18) and (A-23) respectively and simplifying the result with (16), we obtain

$$\begin{aligned} [{}_B R_1(y)]_t &= \left[ {}_B R_1(y) + 2(\beta_C - 1) \right. \\ &\quad + \sqrt{(2/\pi)} y_t (1 + \sigma_A^2) \exp(-y_t^2/2) \\ &\quad - \frac{4}{\pi} \left\{ \sigma_B^2 [\exp(-y_t^2/2\sigma_B^2) - 1] \right. \\ &\quad \left. - \sigma_A \sqrt{\pi} \int_0^{y_t^2/2} \sqrt{u} \exp(-u) \right. \\ &\quad \left. \times \operatorname{erf}\left(\frac{\sigma_A}{\sigma_B} \sqrt{u}\right) du \right\} \Big] \\ &\quad \times [\beta_C + \sqrt{(2/\pi)} y_t \exp(-y_t^2/2)]^{-1}. \end{aligned} \quad (31)$$

${}_B R_1(y)$  in (31) is given by (SP, 1976)

$$\begin{aligned} {}_B R_1(y) &= \langle (y_N - y_p^c)^2 \rangle / \langle y_N^2 \rangle = \langle (y_N - y_p^c)^2 \rangle \\ &= 2 - \frac{4}{\pi} [\sigma_B + \sigma_A \sin^{-1}(\sigma_A)]. \end{aligned} \quad (32)$$

*Index*  $[{}_B R_1(z)]_t$ . From the definition of  $[{}_B R_1(z)]_t$  given in Table 1 we can write

$$[{}_B R_1(z)]_t = \frac{\langle y_N^4 \rangle_t + \langle (y_p^c)^4 \rangle_t - 2\langle y_N^2 (y_p^c)^2 \rangle_t}{\langle y_N^4 \rangle_t}. \quad (33)$$

Substituting for  $\langle y_N^4 \rangle_t$ ,  $\langle (y_p^c)^4 \rangle_t$  and  $\langle y_N^2 (y_p^c)^2 \rangle_t$  from (A-15), (A-22) and (A-24) respectively and simplifying, we obtain

$$\begin{aligned} [{}_B R_1(z)]_t &= \{{}_B R_1(z) + \sqrt{(2/\pi)} (1 - \sigma_A^2) (y_t/3\beta_C) \\ &\quad \times \exp(-y_t^2/2) [(1 + y_t^2) \\ &\quad + \sigma_A^2 (3 - y_t^2)]\} [1 + \sqrt{(2/\pi)} (y_t/3\beta_C) \\ &\quad \times (3 + y_t^2) \exp(-y_t^2/2)]^{-1}. \end{aligned} \quad (34)$$

In obtaining (34) we have used (16) as well as the result (SP, 1976)

$${}_B R_1(z) = \frac{4}{3} \sigma_B^2. \quad (35)$$

*Index*  $[R_1^f(y)]_t$ . From the definition of  $[R_1^f(y)]_t$  given in Table 1, we can write

$$[R_1^f(y)]_t = 2 \int_{y_t}^{\infty} \int_0^{\infty} \left| \frac{y_N - y_p^c}{y_N + y_p^c} \right| P_t(y_N, y_p^c) dy_N dy_p^c. \quad (36)$$

With (13) we can rewrite (36) as

$$\begin{aligned} [R_1^f(y)]_t &= \frac{1}{\beta_C} \left[ 2 \int_0^{\infty} \int_0^{\infty} \left| \frac{y_N - y_p^c}{y_N + y_p^c} \right| P(y_N, y_p^c) dy_N dy_p^c \right. \\ &\quad \left. - 2 \int_0^{y_t} \int_0^{\infty} \left| \frac{y_N - y_p^c}{y_N + y_p^c} \right| \right. \\ &\quad \left. \times P(y_N, y_p^c) dy_N dy_p^c \right]. \end{aligned} \quad (37)$$

The first term within the square brackets represents  $R_1^f(y)$  (see PP, 1977). Making use of the transformation (24) in the integrals occurring as the second term on the right-hand side of (37), we obtain

$$\begin{aligned} [R_1^f(y)]_t &= \frac{1}{\beta_C} \left[ R_1^f(y) - 2 \int_0^{y_t/(1+y_t)} \int_0^1 \left| \left( \frac{u}{1-u} \right. \right. \right. \\ &\quad \left. \left. \left. - \frac{v}{1-v} \right) \right| \left( \frac{u}{1-u} + \frac{v}{1-v} \right) \right. \\ &\quad \left. \times P\left( \frac{u}{1-u}, \frac{v}{1-v} \right) \right. \\ &\quad \left. \times \frac{du}{(1-u)^2} \frac{dv}{(1-v)^2} \right]. \end{aligned} \quad (38)$$

$R_1^f(y)$  has been shown to be (PP, 1977)

$$R_f^I(\mathcal{Y}) = \frac{2}{\pi} \left\{ [(1 + \sigma_A)/(1 - \sigma_A)]^{1/2} \ln [2/(1 + \sigma_A)] \right. \\ \left. - [(1 - \sigma_A)/(1 + \sigma_A)]^{1/2} \ln [2/(1 - \sigma_A)] \right\}. \quad (39)$$

*Index*  $[R_1^f(z)]_t$ . From the definition of  $[R_1^f(z)]_t$  given in Table 1 we can write

$$[R_1^f(z)]_t = 2 \int_{y_t}^{\infty} \int_0^{\infty} \left| \frac{y_N^2 - (y_p^c)^2}{y_N^2 + (y_p^c)^2} \right| P_t(y_N, y_p^c) dy_N dy_p^c. \quad (40)$$

Following the same procedure as that used for  $[R_1^f(y)]_t$ , we can show that (40) becomes

$$[R_1^f(z)]_t = \frac{1}{\beta_c} \left[ R_1^f(z) - 2 \int_0^{y_t/(1+y_t)} \int_0^1 \left[ \left( \frac{u}{1-u} \right)^2 - \left( \frac{v}{1-v} \right)^2 \right] / \left[ \left( \frac{u}{1-u} \right)^2 + \left( \frac{v}{1-v} \right)^2 \right] P \left( \frac{u}{1-u}, \frac{v}{1-v} \right) \times \frac{du}{(1-u)^2} \frac{dv}{(1-v)^2} \right], \quad (41)$$

Table 2. Values of  $[R_1(y)]_t$  and  $[R_1(z)]_t$  as functions of  $\sigma_A$  and  $y_t$  for the centrosymmetric case

$[R_i(y)]_i$						$[R_j(z)]_i$						
$\sigma_A$	$y_i \rightarrow$	0.00	0.15	0.30	0.45	0.60	$y_i \rightarrow$	0.00	0.15	0.30	0.45	0.60
0.000	82.843	72.763	65.864	61.396	58.779	127.324	115.981	105.008	96.268	89.576		
0.040	82.786	72.715	65.823	61.360	58.745	127.222	115.948	104.942	96.217	89.535		
0.080	82.616	72.551	65.701	61.233	58.646	126.916	115.249	104.744	96.061	89.410		
0.120	82.331	72.331	65.497	61.074	58.479	126.404	114.831	104.412	95.800	89.201		
0.160	81.930	71.993	65.209	60.821	58.243	125.684	114.243	103.945	95.532	88.903		
0.200	81.510	71.554	64.943	60.482	57.936	124.753	113.649	103.337	94.951	88.515		
0.240	80.768	71.012	64.373	60.085	57.535	123.603	112.939	102.584	94.514	88.029		
0.280	80.000	70.363	63.819	59.596	57.096	122.231	111.413	101.681	93.634	87.440		
0.320	77.100	69.602	63.169	59.021	56.556	120.629	110.094	100.619	92.783	86.740		
0.360	78.061	68.723	62.417	58.355	55.928	118.787	108.573	99.389	91.791	85.917		
0.400	76.876	67.720	61.557	57.591	55.205	116.694	106.838	97.980	90.646	84.960		
0.420	76.422	67.169	61.085	57.169	54.806	115.550	105.887	97.203	90.013	84.427		
0.440	75.536	66.582	60.582	56.723	54.379	114.337	104.876	96.377	89.335	83.854		
0.460	74.803	65.962	60.047	56.243	53.924	113.053	103.805	95.497	88.611	83.240		
0.480	74.727	65.303	59.480	55.732	53.440	111.697	102.670	94.563	87.839	82.581		
0.500	73.705	64.605	58.878	55.193	52.923	110.266	101.469	93.571	87.015	81.874		
0.520	72.336	63.864	58.240	52.623	51.373	108.756	100.192	92.518	86.137	81.117		
0.540	71.416	63.084	57.564	52.044	50.888	107.164	98.857	91.401	85.201	80.306		
0.560	70.444	62.236	56.848	52.365	50.164	105.487	97.439	90.216	84.203	79.436		
0.580	69.515	61.343	56.089	52.671	50.500	103.720	95.940	88.958	82.139	78.504		
0.600	68.320	60.453	55.284	51.946	49.792	101.829	94.236	87.624	82.004	77.504		
0.620	67.161	59.949	54.500	49.930	49.053	100.892	93.231	86.927	81.009	76.977		
0.640	66.378	58.949	53.744	49.234	48.030	99.879	92.063	86.208	80.792	76.433		
0.660	65.993	58.047	52.964	48.534	47.030	98.839	90.913	85.458	80.447	76.865		
0.680	65.647	57.236	52.169	47.869	45.568	97.823	90.970	84.704	79.999	75.278		
0.700	65.300	56.467	51.406	47.209	44.268	96.828	89.920	83.075	78.447	74.637		
0.720	64.993	55.747	50.736	46.569	42.944	95.829	88.020	82.205	77.302	73.362		
0.740	64.694	55.093	50.069	45.904	40.650	94.833	86.126	81.510	76.543	72.402		
0.760	64.398	54.447	49.406	45.246	39.938	93.833	84.226	80.262	75.445	71.261		
0.780	64.101	53.809	48.771	44.634	38.509	90.921	83.452	78.538	75.107	70.498		
0.800	63.815	53.161	48.124	44.071	37.978	89.938	81.636	74.238	70.494	69.704		
0.820	63.528	52.513	47.475	43.429	36.628	88.360	82.718	77.651	73.338	69.817		
0.840	63.242	51.863	46.826	42.804	35.326	87.039	81.341	75.578	71.499	68.017		
0.860	62.957	51.213	46.175	42.164	34.039	85.339	80.341	74.486	70.526	67.121		
0.880	62.670	50.569	45.524	41.517	32.751	84.217	79.093	74.486	70.526	67.121		
0.900	62.384	50.000	44.873	40.877	31.471	82.751	77.805	73.354	69.514	66.185		
0.920	62.097	49.333	44.223	40.233	30.188	81.238	76.472	72.179	68.660	65.209		
0.940	61.811	48.684	43.573	39.604	28.907	79.677	75.092	70.960	67.363	64.189		
0.960	61.524	48.016	42.914	40.033	27.538	78.063	73.663	69.693	66.218	63.122		
0.980	61.238	47.359	42.262	39.453	26.181	76.394	72.181	68.374	65.072	62.005		
0.800	60.953	46.713	41.605	38.836	24.896	74.667	70.642	67.000	63.772	60.833		
0.820	60.668	46.068	40.953	38.205	23.596	72.876	69.042	65.567	62.463	59.603		
0.840	60.382	45.422	40.301	37.575	22.372	71.017	67.376	64.070	61.090	58.310		
0.860	60.096	44.767	39.651	36.907	21.107	69.084	65.639	62.503	59.648	56.948		
0.880	59.810	44.111	38.903	36.250	20.839	67.072	63.825	60.859	58.130	55.511		
0.900	59.524	43.454	38.153	35.602	19.567	64.973	61.926	59.132	56.529	53.992		
0.920	59.238	42.797	37.404	34.953	19.297	62.777	59.933	57.312	54.834	52.381		
0.940	58.952	42.141	36.756	34.305	18.027	60.476	57.835	55.389	53.037	50.668		
0.960	58.666	41.485	36.108	33.656	17.756	58.055	55.527	53.350	51.124	48.842		
0.980	58.380	40.833	35.460	33.007	17.486	55.499	53.274	51.179	49.079	46.887		
0.900	58.094	40.187	34.812	32.355	17.216	52.427	50.046	48.038	46.002	45.856		
0.920	57.808	39.540	34.164	31.705	16.946	50.790	48.776	46.857	44.883	44.785		
0.940	57.522	38.883	33.516	31.057	16.677	49.136	47.662	45.634	43.721	43.672		
0.960	57.236	38.235	32.868	30.409	16.408	47.500	45.492	43.457	41.511	41.513		
0.980	56.950	37.588	32.227	29.761	16.139	45.823	43.466	41.300	39.439	40.039		
0.900	56.664	36.941	31.580	29.104	15.870	44.155	42.367	40.347	38.714	38.714		
0.920	56.378	36.294	30.933	28.447	15.601	42.597	40.477	38.456	36.732	36.732		
0.940	56.092	35.647	30.285	27.790	15.332	41.030	39.244	37.223	35.505	35.505		
0.960	55.806	35.000	30.638	27.133	15.063	39.473	38.031	36.010	34.291	34.291		
0.980	55.520	34.353	29.982	26.475	14.794	37.812	36.619	34.589	32.868	32.868		
0.900	55.234	33.706	29.335	25.817	14.525	36.251	35.008	32.987	31.266	31.266		
0.920	54.948	33.059	28.688	25.150	14.256	34.684	33.797	31.675	30.955	30.955		
0.940	54.662	32.412	28.041	24.483	13.987	33.123	32.535	30.413	29.692	29.692		
0.960	54.376	31.765	27.394	23.814	13.718	31.554	31.944	29.822	28.991	28.991		
0.980	54.090	31.118	26.747	23.147	13.449	30.983	31.333	29.199	28.377	28.377		
0.900	53.804	30.471	26.100	22.475	13.180	29.412	29.741	27.619	26.798	26.798		
0.920	53.518	29.813	25.453	21.794	12.911	28.841	29.170	27.098	26.275	26.275		
0.940	53.232	29.166	24.766	21.127	12.642	28.270	28.599	26.527	25.604	25.604		
0.960	52.946	28.519	24.119	20.450	12.373	27.699	27.998	25.926	24.993	24.993		
0.980	52.660	27.872	23.472	19.773	12.104	27.128	27.427	25.355	24.332	24.332		
0.900	52.374	27.225	22.825	19.096	11.835	26.557	26.856	24.784	23.761	23.761		
0.920	52.088	26.578	22.178	18.428	11.566	25.986	26.285	24.213	23.190	23.190		
0.940	51.802	25.931	21.531	17.761	11.307	25.415	25.714	23.641	22.518	22.518		
0.960	51.516	25.284	20.884	17.084	11.038	24.844	25.143	23.068	21.940	21.940		
0.980	51.230	24.637	20.206	16.406	10.767	24.273	24.572	22.500	21.377	21.377		
0.900	50.944	24.090	19.549	15.727	10.500	23.702	24.001	21.929	20.800	20.800		
0.920	50.658	23.443	18.893	15.050	10.233	23.131	23.430	21.358	20.231	20.231		
0.940	50.372	22.796	18.246	14.373	9.959	22.560	22.859	20.787	19.666	19.666		
0.960	50.086	22.149	17.608	13.694	9.684	21.989	22.288	20.216	19.093	19.093		
0.980	49.800	21.502	17.021	13.017	9.417	21.428	21.727	19.644	18.521	18.521		
0.900	49.514	20.855	16.355	12.340	9.150	20.857	21.156	19.073	17.950	17.950		
0.920	49.228	20.208	15.698	11.647	8.883	20.287	20.586	18.504	17.381	17.381		
0.940	48.942	19.561	15.041	11.022	8.610	19.717	20.015	18.032	16.909	16.909		
0.960	48.656	18.914	14.374	10.395	8.337	19.146	19.445	17.462	16.340	16.340		
0.980	48.370	18.267	13.717	10.000	8.054	18.575	18.874	16.891	15.769	15.769		
0.900	48.084	17.620	13.050	9.714	7.771	17.994	18.293	16.300	15.178	15.178		
0.920	47.798	16.963	12.383	9.427	7.508	17.423	17.722	15.739	14.617	14.617		
0.940	47.512	16.306	11.716	9.140	7.234	16.852	17.151	15.168	14.045	14.045		
0.960	47.226	15.649	11.043	8.853	6.961	16.281	16.580	14.598	13.477	13.477		
0.980	46.940	15.000	10.376	8.573	6.680	15.710	16.009	14.027	12.905	12.905		
0.900	46.654	14.343	9.733	8.294	6.400	15.139	15.438	13.456	12.334	12.334		
0.920	46.368	13.686	9.166									

where  $R_1^f(z)$  is given by (PP, 1977)

$$R_1^f(z) = \frac{2\sigma_B}{\pi\sigma_A} \ln \left( \frac{1 + \sigma_A}{1 - \sigma_A} \right). \quad (42)$$

### **3. Discussion of the theoretical results**

The theoretical expressions for the six normalized  $R$  indices valid for truncated data have been derived in (25), (29), (31), (34), (38) and (41). A study of these equations shows that we can, in general, write the  $R$  indices applicable to the truncated data in the general form as

$$[R]_t = A(y_t) [R + B(\sigma_A, y_t)], \quad (43)$$

where  $R$  stands for any one of the normalized  $R$  indices,  $A(y_t)$  is a function of  $y_t$  and  $B(\sigma_A, y_t)$  is a function of  $\sigma_A$  and  $y_t$ . If  $y_t \rightarrow 0$ ,  $A(y_t) \rightarrow 1$  and  $B(\sigma_A, y_t) \rightarrow 0$  so that  $[R]_t \rightarrow R$  as required.

A study of (25), (29), (31), (34), (38) and (41) shows that these  $R$  indices depend on the parameters  $y_t$  (which is a characteristic of the data) and  $\sigma_A$ .  $\sigma_A$  is in turn a function of  $\sigma_1^2$  (*i.e.* the fractional contribution to the local mean intensity from the known atoms),  $\langle |\Delta\mathbf{r}| \rangle$  (*i.e.* the mean positional error in the atoms of the model) and  $\sin \theta/\lambda$ . Putting  $\sigma_A = \sigma_1$  (*i.e.*  $\langle |\Delta\mathbf{r}| \rangle = 0$ ) in these equations, we can obtain the results for the related case. Similarly, putting  $\sigma_A = 0$  (*i.e.*  $\langle |\Delta\mathbf{r}| \rangle$  large), we can obtain the results for the unrelated case. The local values of these  $R$  indices (in percent) are given in Tables 2-4 as functions of  $\sigma_A$  for different fixed values of  $y_t$ ,

Table 3. Values of  $[{}_B R_1(y)]$ , and  $[{}_B R_1(z)]$ , as functions of  $\sigma_A$  and  $y$ , for the centrosymmetric case

$\sigma_4$	$y_t \rightarrow 0.00$	$ {}_B R_1(z) _t$	$y_t \rightarrow 0.00$	$ {}_B R_1(z) _t$
0.000	72.676	62.143	54.377	49.045
0.040	72.774	62.059	54.307	48.085
0.080	72.268	61.885	54.097	48.804
0.120	71.558	61.785	53.746	45.479
0.160	71.932	60.974	53.293	45.205
0.200	70.623	60.031	52.677	44.820
0.240	68.952	59.926	51.537	44.322
0.280	67.952	59.796	50.909	43.709
0.320	66.100	59.670	49.831	45.123
0.360	64.333	59.523	48.601	44.055
0.400	62.347	59.326	47.214	42.849
0.440	61.271	59.168	46.460	42.192
0.480	60.140	59.174	45.666	41.499
0.520	59.851	50.754	44.830	40.768
0.560	57.705	49.715	43.951	39.998
0.600	56.401	48.626	43.029	39.190
0.640	55.338	47.487	42.063	38.341
0.680	53.316	46.297	41.053	37.451
0.720	52.332	45.054	39.996	36.518
0.760	50.588	43.759	38.892	35.542
0.800	48.981	42.410	37.170	34.520
0.840	48.154	41.714	37.145	33.992
0.880	47.310	41.005	36.538	33.452
0.920	46.451	40.281	35.917	32.900
0.960	45.575	39.543	35.284	32.336
0.650	44.682	38.791	34.638	31.759
0.690	43.773	38.924	33.978	31.169
0.730	42.846	37.242	33.305	30.566
0.770	41.903	36.444	32.617	29.950
0.810	40.942	35.632	31.916	29.320
0.850	39.964	34.804	31.200	28.677
0.890	38.968	33.960	30.469	28.019
0.930	37.953	33.100	29.723	27.346
0.970	36.921	32.223	28.962	26.659
0.740	35.869	31.330	28.186	25.956
0.780	34.799	30.419	27.393	25.237
0.820	33.710	29.492	26.583	24.502
0.860	32.601	28.546	25.757	23.751
0.900	31.472	27.583	24.913	22.982
0.940	30.322	26.601	24.052	22.195
0.800	29.152	25.599	23.172	21.391
0.840	27.961	24.579	22.273	20.567
0.880	26.748	23.538	21.355	19.723
0.920	25.512	22.477	20.416	18.859
0.840	24.254	21.394	19.456	17.974
0.880	22.973	20.290	18.474	17.067
0.920	21.667	19.162	17.470	16.136
0.870	20.336	18.011	16.442	15.182
0.880	18.979	16.836	15.388	14.202
0.890	17.596	15.635	14.308	13.196
0.900	16.185	14.406	13.201	12.161
0.905	15.468	13.782	12.636	11.633
0.910	14.744	13.150	12.064	11.097
0.915	14.012	12.510	11.483	10.554
0.920	13.273	11.863	10.895	10.002
0.925	12.525	11.207	10.298	9.442
0.930	11.769	10.543	9.692	8.874
0.935	11.004	9.871	9.077	8.296
0.940	10.230	9.189	8.452	7.710
0.945	9.447	8.498	7.817	7.114
0.950	8.654	7.979	7.171	6.509
0.955	7.851	7.085	6.514	5.894
0.960	7.038	6.362	5.845	5.269
0.965	6.213	5.627	5.163	4.634
0.970	5.375	4.879	4.468	3.990
0.975	4.525	4.116	3.758	3.337
0.980	3.660	3.337	3.033	2.676
0.985	2.779	2.540	2.293	2.009
0.990	1.880	1.721	1.537	1.339
0.995	0.957	0.875	0.770	0.669
1.000	0.000	0.000	0.000	0.000

since these are needed for evaluating the overall values of the  $R$  indices for a given situation (see later).

The variations of the  $R$  indices as a function of  $y_t$  for different fixed values of  $\sigma_1^2$  have been obtained with the results in Tables 2-4 and the results obtained are shown in Figs. 1(a)-1(f). These figures have been obtained for the typical case where  $\langle |\Delta r| \rangle = 0.2 \text{ \AA}$  and  $\sin \theta/\lambda = 0.4 \text{ \AA}^{-1}$ . From a study of these figures, we obtain the following results. (i) As  $y_t$  increases the value of  $R$  decreases. However, for  $y_t > 0.3$  this decrease is less marked. (ii) The decrease in  $R$  with  $y_t$  is more marked when  $\sigma_1^2$  is small than when it is close to unity. Since for the data of actual crystals  $y_t$  is expected to be in the neighbourhood of 0.2 (Ponnuswamy & Parthasarathy,

1977), it would be useful to take care of data truncation for the calculation of the theoretical overall values of  $R$  indices. In view of (ii) this is particularly true for incomplete models.

We shall summarize here the general procedure that may be followed for computing the theoretical overall values of  $R$  for a given model. During the structure completion stage, since the atoms added to the model are subject to positional errors of the order of  $0.2 \text{ \AA}$  on average, one may set  $\langle |\Delta r_i| \rangle \simeq 0.2 \text{ \AA}$ . The evaluation of  $[\bar{R}]_t$  involves the following steps. (i) From an analysis of the  $F_o$  data, determine the value of  $y_t$  appropriate to the data. (ii) Determine  $\sigma_i^2$  for the given model. For a structure with similar atoms this may be taken to be

Table 4. Values of  $[R_j^f(y)]$ , and  $[R_j^f(z)]$ , as functions of  $\sigma_4$  and  $y_t$  for the centrosymmetric case

$\sigma_A$	$y_t \rightarrow 0.00$	$0.15$	$0.30$	$0.45$	$0.60$	$y_t \rightarrow 0.00$	$0.15$	$0.30$	$0.45$	$0.60$
0.000	88.254	80.165	76.974	76.335	77.357	127.324	120.338	116.383	114.867	115.321
0.040	88.423	80.023	76.942	76.301	77.319	127.290	120.301	116.345	114.827	115.277
0.080	88.579	80.026	76.844	76.199	77.205	127.188	120.191	116.345	114.709	115.147
0.120	87.748	79.673	76.681	76.028	77.113	127.016	120.006	116.041	114.509	114.247
0.160	87.447	79.643	76.521	75.786	75.742	126.773	119.749	115.777	114.227	114.015
0.200	87.057	78.972	76.420	75.980	75.948	126.526	119.403	115.498	113.999	114.209
0.240	86.662	78.555	75.258	74.607	74.548	126.061	118.929	115.981	113.701	114.087
0.280	86.119	75.957	74.798	74.049	74.474	125.529	118.626	115.216	112.166	114.250
0.320	85.555	77.395	74.181	72.938	74.053	124.559	117.142	113.869	110.416	114.202
0.360	84.862	76.023	73.760	72.646	72.203	123.939	116.946	113.445	110.223	114.228
0.400	84.074	76.023	73.655	72.430	72.225	123.568	116.568	113.269	109.465	109.921
0.440	83.674	75.498	72.506	71.284	71.584	123.223	116.254	113.048	108.308	108.029
0.480	83.372	74.941	71.726	70.307	71.104	122.700	115.929	112.951	107.561	107.701
0.520	82.675	74.322	71.214	70.253	70.485	122.139	115.691	112.653	106.946	106.502
0.560	82.145	73.889	70.667	69.671	69.822	120.839	113.047	108.864	105.505	105.191
0.600	81.580	73.311	70.085	69.049	69.112	119.896	112.358	108.153	105.380	105.945
0.640	80.976	72.693	69.463	68.384	68.353	119.206	111.619	107.301	105.759	103.759
0.680	80.331	72.034	68.798	67.673	67.539	118.467	110.827	106.573	104.509	102.700
0.720	79.641	71.330	68.088	66.911	66.666	117.672	109.977	105.696	103.573	102.023
0.760	79.279	70.960	67.715	66.510	65.729	117.253	109.528	105.233	103.078	102.101
0.800	78.903	70.577	67.328	66.094	65.243	116.818	109.063	104.752	102.293	100.953
0.840	78.515	70.181	66.929	65.664	64.721	116.366	108.580	104.254	102.029	100.707
0.880	78.112	69.771	66.514	65.217	64.188	115.897	108.079	103.736	101.474	100.323
0.920	77.696	69.347	66.085	64.754	63.635	115.10	107.558	103.198	100.897	99.668
0.960	77.263	68.907	65.440	64.273	63.476	114.903	107.017	102.639	100.296	98.986
0.670	76.815	68.451	65.179	63.774	63.061	114.576	106.454	102.058	99.671	98.275
0.700	76.350	67.978	64.700	63.255	62.463	113.827	105.869	101.453	97.533	96.760
0.730	75.867	67.487	64.203	62.716	61.842	113.255	105.239	100.822	98.339	96.670
0.770	75.364	66.977	63.586	62.154	61.195	112.659	104.624	100.165	97.629	95.952
0.810	74.842	66.448	63.149	61.570	60.521	112.037	103.961	99.480	96.888	95.107
0.850	74.299	65.897	62.590	60.960	59.816	111.388	103.269	98.764	96.113	94.223
0.890	73.733	65.323	62.008	60.324	59.086	110.2546	98.015	95.301	93.298	92.347
0.930	73.143	64.726	61.400	59.960	58.320	109.997	101.790	97.232	94.450	92.347
0.970	72.527	64.102	60.766	58.966	57.520	109.252	100.997	96.411	93.557	91.399
0.780	71.883	63.452	60.103	58.239	56.682	108.470	100.167	95.549	92.619	90.239
0.820	71.209	62.771	59.100	57.477	55.804	107.649	99.294	96.644	91.631	89.113
0.860	70.504	62.059	58.683	56.677	54.884	106.784	98.377	93.692	90.590	87.927
0.900	69.763	61.313	57.920	55.835	53.917	105.873	97.410	92.687	89.490	86.675
0.940	68.985	60.529	57.118	54.949	52.900	104.910	96.390	91.626	88.327	85.351
0.980	68.165	59.704	56.473	54.014	51.828	103.891	95.310	90.503	87.093	83.950
0.820	67.300	58.835	55.380	53.025	50.697	102.809	94.167	89.312	85.782	82.663
0.860	66.386	57.917	54.436	51.977	49.502	101.660	92.951	88.044	84.385	80.882
0.900	65.416	56.925	53.434	50.863	48.237	100.433	91.656	86.691	82.892	79.198
0.940	64.385	55.913	52.368	49.676	46.894	99.121	90.272	85.244	81.293	77.399
0.980	63.286	54.814	51.229	48.408	45.465	97.712	88.788	83.688	79.572	75.472
0.870	62.108	53.638	50.008	47.047	43.942	96.192	87.189	82.010	77.714	73.403
0.920	60.842	52.376	48.594	45.582	42.314	94.566	85.458	80.190	75.699	71.172
0.960	59.974	51.015	47.271	43.997	40.569	92.752	83.576	78.206	73.503	68.760
0.990	57.987	49.538	45.721	42.274	38.693	90.786	81.516	76.029	71.096	66.139
0.930	57.192	48.749	44.892	41.354	37.700	89.727	80.408	74.856	69.801	64.742
0.970	56.358	47.923	44.021	40.391	36.669	88.612	79.242	73.620	68.439	63.280
0.910	55.483	47.056	43.105	39.380	35.595	87.435	78.013	72.313	67.003	61.749
0.950	54.561	46.145	42.140	38.318	34.477	86.188	76.712	70.929	65.485	60.143
0.990	53.587	45.182	41.119	37.199	33.311	84.864	75.331	69.459	63.877	58.452
0.935	52.554	44.164	40.036	36.018	32.094	83.453	73.861	67.890	62.170	56.678
0.975	51.457	43.081	38.883	34.769	30.822	81.943	72.290	66.211	60.351	54.804
0.915	50.285	41.927	37.651	33.444	29.491	80.319	70.603	64.405	58.408	52.823
0.955	49.027	40.690	36.327	32.035	28.096	78.566	68.783	62.455	56.329	50.722
0.995	47.670	39.356	34.900	30.531	26.633	76.559	66.806	60.335	54.082	48.488
0.935	46.196	37.909	33.349	28.922	25.094	74.571	64.644	58.016	51.655	46.104
0.975	45.581	36.324	31.654	27.193	23.473	72.264	62.258	55.459	49.019	43.543
0.915	42.794	34.572	29.784	25.326	21.760	69.686	59.596	52.613	46.129	40.792
0.955	40.790	32.608	27.702	23.301	19.944	66.766	56.584	49.408	42.935	37.804
0.995	38.504	30.368	25.352	21.088	18.003	63.395	53.111	45.745	39.374	34.523
0.935	38.831	27.349	22.661	18.649	15.909	59.402	49.002	41.479	35.342	30.871
0.975	35.591	24.573	19.513	15.919	13.603	54.483	43.949	36.376	30.670	26.720
0.995	28.412	20.486	15.714	12.766	10.960	48.018	37.335	30.004	25.041	21.812
1.000	22.278	14.602	10.819	8.801	7.654	38.271	27.351	21.325	17.647	15.233

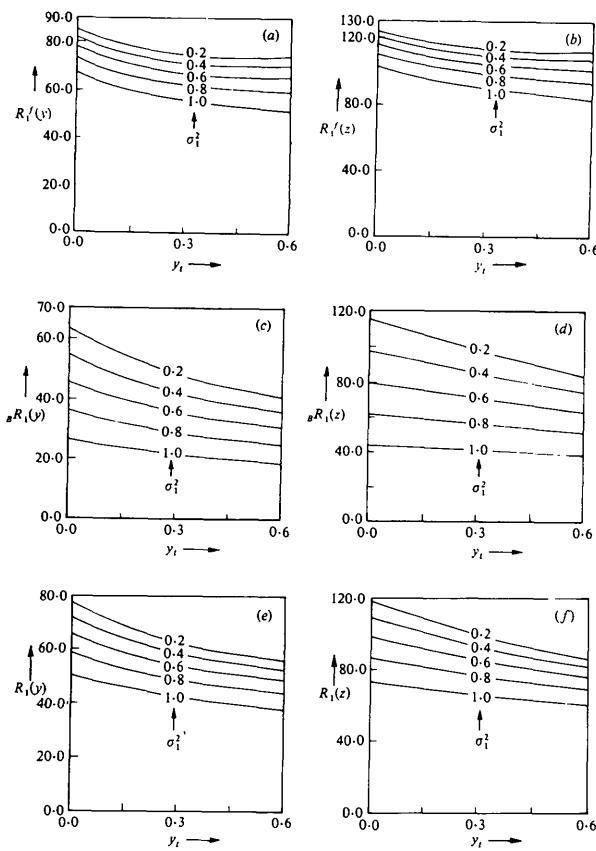


Fig. 1. Variation of the local values of normalized  $R$  indices as a function of  $y_t$  for different fixed values of  $\sigma_i^2$ . For the definition of  $R_1(y)$ ,  $R_1(z)$ , etc., see column 6 of Table 1.

P/N. (iii) Divide the range  $0 \leq s \leq S_{\max}$  into a number of narrow subintervals. Determine from the data the number ( $n_s$ ) of observed reflections in each of these sub-intervals. (iv) From the mean value of  $\sin \theta/\lambda$  corresponding to each sub-interval determine the values of  $f$ . (v) Calculate  $\sigma_A$  (by taking  $\langle |\Delta r| \rangle = 0.2 \text{ \AA}$ ) corresponding to each of these sub-intervals. (vi) Make use of the results in Tables 2–4 and determine the values of  $[R]_t$  for these sub-intervals by bilinear interpolation. (vii) Make use of the results thus obtained in the appropriate expressions for  $[\bar{R}]_t$  and compute the overall values  $[\bar{R}]_t$ . The values thus obtained represent the theoretical overall values of the normalized  $R$  indices corresponding to a model for which  $\langle |\Delta r| \rangle = 0.2 \text{ \AA}$  and for data in which  $y_N \geq y_t$  and  $0 \leq s \leq S_{\max}$ .

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## Theoretical Evaluation of the Overall Values of Discrepancy Indices for Truncated Data. II. Normalized $R$ indices for a Non-centrosymmetric Crystal with Similar Atoms

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### Abstract

Theoretical expressions and numerical tables for the local values of six types of normalized  $R$  indices are obtained for an imperfectly related incomplete model of

a non-centrosymmetric crystal with truncated data. Under similar conditions, the curve of the local value of an  $R$  index versus the truncation limit  $y_t$  is relatively more flat for the non-centrosymmetric case than for the centrosymmetric case particularly in the region where  $y_t$  is small.

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